Simulation Analysis of Equivalent Circuit Model of Skin-Electrode Impedance

Submission date: 03-May-2021 07:58PM (UTC+0700) Submission ID: 1576739895 File name: Camera_Ready_Paper_to_BEEI_2021_03052021.pdf (509.37K) Word count: 4042 Character count: 21909 Bulletin of Electrical Engineering and Informatics Vol. X, No. X, May 2021, pp. ab~cd ISSN: 2302-9285, DOI: 10.11591/eei.v8i4.xxxx

1

Simulation Analysis of Equivalent Circuit Model of Skin-Electrode Impedance for Transcutaneous Electrical Stimulation

Joni W 14 an Simatupang¹, Wilbert Wijaya¹, David Tyler² and Clementine Mavridis² ¹Electrical Engineering Study Program, Faculty of Engineering, Presid 22 University, Cikarang, Indonesia ²Fashion Institute, Manchester Metropolitan University (MMU), Manchester, United Kingdom

Article Info Article history:

ABSTRACT

Received X X, 2021 Revised X X, 2021 Accepted X X, 2021

Keywords:

Electrical stimulation Transcutaneous Impedance Capacitive Resistive For more than 50 years, transcutaneous electrical stimulation method has been used to cure the spinal cord injury, stroke or cerebral palsy. This method works by activating the excitable nerves, muscle fibers by electrical current stimulation through electrode interface to skin. Electrode to skin interface requires equivalent circuit to overcome the inability of measuring the skin resistivity directly. Therefore, equivalent circuit inside the E-textile must be modelled properly for it to represents the skin nature, which is resistive and capacitive. We have been learned several models after the skin from previous works, which are from Lawler, Moineau and Keller & Kuhn. Unfortunately, Moineau model neglects the capacitance effect (we then neglected this model in our simulation analysis), while Lawler and Keller and Kuhn include capacitive and resistive nature of skin in their equivalent circuits. Both models consisted of only one parallel RC block. This paper presents the simulation results of the proposed equivalent circuit model using two parallel RC circuits. Simulation of the proposed model is conducted in MATLAB 2015a and compared with two previous models (Lawler and Keller & Kuhn) using certain parameters. The results show that the proposed model obtained the impedance of 10.830 k Ω when it is simulated using 100Hz of frequency, for Lawler et.al model the impedance is 5.340 k Ω and Keller & Kuhn model the impedance obtained is 6.490 kΩ. Therefore, the proposed model has the refined impedance compared with other models and is expected to deliver better electrical stimulation.

> Copyright © 2020 Institute of Advanced Engineering and Science. All rights reserved.

Corresponding Author:

Joni Welman Simatupang, Bectrical Engineering Study Program, Faculty of Engineering, President University, Jababeka Education Park, Cikarang, Bekasi 17530 - Indonesia, Email: joniwsmtp@president.ac.id

1. INTRODUCTION

Wearable Transcutaneous Electrical Stimulation (TES) or Functional Electrical Stimulation (FES) is the method used to cure motoric injury due to stroke, spinal cord injury, or cerebral palsy, by activating excitable tissue from skin surface [1], [2]. This feethod has been applied in curing those diseases for > 50 years [3]. TES or FES also works by activating the nerves and muscle fibers by stimulation using electrical current pulses through two electrodes and using inter-electrode distance (IED) which attached on the skin [4].

Journal homepage : http://beei.org/index.php/EEI/

Electrical stimulation can be applied effectively for skin restoration, diagnosis and treatment purpose, by application of artificial tactile sensory feedback in prosthetic hand [5], [6]. Application of electrical stimulation requires highly reliable electrode, sustainable, and low-cost electrode material. Textile electrode fulfills these criteria as electrode material with price at £0.16 per electrode, which also provides high measure 11 nt accuracy and reusability [7]. Textile electrode is also providing flexibility, ventilation that can lead to almost no skin irritation for long-term usage, foldation and non-hydrogel characteristics. Textile electrodes is applicable for monitoring clinical physiological signals, such as electrocardiogram (ECG), electromyography (EMG), electroencephalogram (EEG), and so forth [8].

Textile electrode or e-textile technology has been around for almost a decade. E-textile permits the injection of electrical components, such as, LED, electrodes, to lay on the fabric for it to bring additional value to fabric [9]. The e-textile will be used as for future development of this research as wearable TES device, for this stage the main concern is designing the skin model for it to interface properly with human skin. The skin model design is made based on the skin two main characteristics, such as, resistive and capacitive, applying parallel RC circuit is the way to model after these characteristics. Resistivity of skin cannot be measured directly. Therefore, equivalent network model is used to obtain the skin resistance [2]. On the other hand, skin capacitance is measureable and frequency dependent, which can be measured with a device called Corneometer CM 825 for measurement using mean frequency of 1MHz or Corneometer CM 820 for low frequency measurement (45-75 KHz) [10], [11]. The capacitance effect is useful to detect the hydration state of the skin and for biometric purpose [10 - 12]. Besides knowing the skin nature for stimulation purpose, current density in this stimulation plays a great role on the stimulation efficiency and comfort, due to the skin and electrodes in-homogeneities. High current density, which localized on the skin surface may cause discomfort and the worst case is skin burns [2].

Stimulation comfort on TES device can be improved by varying the waveform and pulse width [1], [5]. On previous research conducted by Baker et.al, they have tried the stimulation using six different types of waveforms such as, asymmetric balanced biphasic square waveform, symmetric biphasic square waveform, monophasic paired spike, modulated sine wave, medium sine wave and medium square wave. Results of their experiment shows that asymmetric biphasic waveform provides better comfort and does not cause any interference or stimulation on large muscle group [13], therefore it is recommended for clinical usage.

Equivalent circuit models have been made to substitute the skin model interface to determine the skin impedance. In this research, we limit to three model as our literature basis. First model was made in 1959 by Lawler et.al using the Wheatstone bridge approach with having both capacitive and resistive components to represents the skin nature. This research shows that impedance is inversely proportional to frequency [14]. Second model made by Keller & Kuhn after the skin equivalent circuit from the skin layers [2]. Third model was made by Moineau et.al, but excluded capacitance effect in their equivalent circuit model [3]. Those approaches yield different results in which, for Moineau et.al design it simply shows no changes in resistance, whereas on Lawler et.al and Keller & Kuhn approach with including both resistive and capacitive nature of skin shows changes on the impedance with respect to frequency. Different equivalent circuit model has their own specialties, and also the waveform used in the stimulation may differ according to each purpose.

Electrode – skin interface is also **p17** ing an important role in electrical stimulation quality because higher impedance electrode will likely having low signal to noise (S/N) ratio, low signal amplitude and poor biological signal quality [15]. But on the other hand, higher electrode impedance may reduce discomfort in stimulation [1]. Increasing the resistivity in the electrode can be done by adding resistive gel, which act as impedance mismatch depletor. Size of electrode is affecting the current density uniformity, by applying electrode with larger contact area (70-120 cm²) may results in high current density and uniform current density, which results from the polarizable electrode characteristics, the displacement current [16].

This research is an extension work of David Tyler and Clementine Mavridis, from Manchester Metropolitan University (MMU), which our concern is in designing the more refined equivalent circuit model [17]. In this paper, the authors propose to simulate the model of Wheatstone bridge, which consists of two identical RC circuit. The RC circuit represents the resistive and capacitive nature of skin. The model will be simulated in MATLAB 2015a, with variation in resistance, capacitance and frequency. Wheatstone bridge approach is considered to be better at approximating the skin impedance, while on the other hand finding the perfect balance impedance in Wheatstone bridge is also more difficult.

2. Human Skin

Human skin is the largest and heaviest organ in the body which contribute 8-10% of human body mass and covers about 2 m^2 of our body's total area. Human skin also serves as boundaries between body and the environment such that, the vital bodily may perform under controlled physiological condition [18 - 20].

Bulletin of Electr Eng and Inf, Vol. X, No. X, May 2021: xx - xx

Ultraviolet (UV) light, chemicals, pathogens and mechanical injury are blocked by skin in first place [21]. Storing water and fats is also part of human skin's function and also serves as immunity to disease [22].

The main structure of human skin are epidemis, dermis and hypodermis [18]. Epidermis consist of several layers, such as, stratum corneum, stratum lucidum, stratum granulosum, stratum spinosum, stratum basale [21]. Dermis is the inner layer of supportive layer of skin, consist of vast amount of collagen and rich in bloce supplies [22]. Hypodermis is the innermost layer of skin, which made up of subcutaneous fat [18]

Stratum corneum is the outermost of epidermis layer, which is the top layer of epidermis and human skin as a whole. Stratum corneum is made up of dead cell, or keratinized cell [4], [21], [22]. It is also one of the thinnest layers which has 15-20 μ m thickness only [23], [24]. Stratum corneum dominates the electronic properties of skin when DC current applied under 10 KHz frequency [4], [23]. Resistivity of Stratum corneum is the highest amongst skin layer at about 10⁵ Ω cm², and conductivity of 0.03 μ F/ cm² at small current application [4], [24].

Dermis is the second main layer of human skin with thickness of 1 to 4 mm, consists of two layers, such as, papillar layer and reticular layer. Papillary layer is the upper layer of dermis, which serves as bo 19 ary to epidermis, loosely connected tissue, with large amount of nerve fibers, capillaries, water and cells. Reticular layer is the bottom part of dermis, which has denser and thicker network compare to papillary layer, houses fewer nerve fibers and capillaries [19].

2.1 Skin Circuit Model

Skin circuit model is required for electrical stimulation due to the immeasurable impedance of it [2]. Making a skin circuit model is the way to simplify our analysis. Skin circuit is modeled by an equivalent circuit, consist of RC circuit. Figure 1 shows the equivalent circuit model of skin [23].

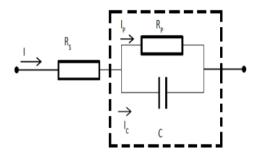


Figure 1. Skin equivalent circuit model.

This skin model is the common way to represent the dielectric properties of skin and skin general response. Analysis of signal input and output from body is simplified with the modelling of this circuit. This model is the most common used for measuring the changes in impedance. In addition, this model is considered to be adequate enough to characterize the skin response [23].

12 In this research the parallel RC circuit will be integrated with Wheatstone bridge circuit which was invented in 1833 by Samuel H. Christie, then improved and popularized by Sir Charles Wheatstone in 1843 [25, 26]. This circuit model is intended to figure out the unknown resistance, using the defined resistance in a bridge model circuit compare with the unknown resistance [26, 27]. This is suitable for measuring skin resistance for it cannot be measured directly. Small changes in resistance can be measured by Wheatstone bridge circuit [26]. Wheatstone bridge can be used for measuring capacitance, inductance, impedance and etc. Wheatstone bridge circuit is used for measuring the unknown parameter for DC source. In balance state, Wheatstone bridge circuit has 0 V voltage across the bridge, therefore, when small changes occur voltage difference exists [25].

2.2 The Previous and Proposed Models

In this part, we will be discussing the skin model made by Lawler et.al, and Keller & Kuhn, and Moineau et.al. First, Lawler et.al proposed the model in 1959 (Fig. 2), stated that skin has both resistive and capacitive nature. They also concluded that impedance of skin will be the same as equivalent circuit in balance condition. Therefore, Lawler et.al come up with the model based of Wheatstone bridge for the skin to have zero voltage in balance state and construct the skin model by using parallel RC circuit, for it to have equal impedance with the skin. This skin model is connected to one of the bridge legs and opposing the electrode.

Simulation Analysis of Equivalent Circuit Model of Skin-Electrode Impedance... (J.W. Simatupang)

(1)

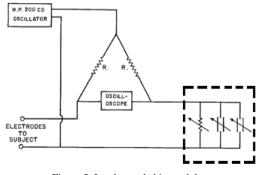


Figure 2. Lawler et.al skin model.

Impedance formula of Lawler et.al model is shown in Equation 1.

$$Z = \frac{R \cdot (\frac{1}{2\pi fC})}{\sqrt{R^2 + (\frac{1}{2\pi fC})^2}}$$

Second, Keller & Kuhn [2] proposed their comprehensive skin model with consist of the matrix and appendageal pathway. The pathways are modeled with resistor and capacitors. In their research, Keller and Kuhn obtained the skin resistivity by tuning the equivalent circuit for yielding the measured current-voltage response. Keller and Kuhn's simple lumped skin model is shown in Figure 3.

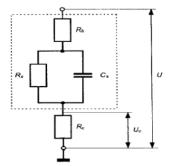


Figure 3. Simple lumped skin model.

The impedance formula of the simple lumped skin model is shown in Equation 2.

$$Z = \frac{R \cdot (\frac{1}{2\pi fC})}{\sqrt{R^2 + (\frac{1}{2\pi fC})^2}} + R_b + R_c$$
(2)

Third, Moineau et al come up with the model only consisting resistive nature of skin, therefore the impedance of the circuit is by using voltage on each node of the circuit (can be solved by using Ohm's law). The results yield without taking account any capacitance effect. In this way we obtained a distorted skin impedance value that can't be comparable with the one of the Wheatstone bridge models [3], [9].

The proposed model is designed based on Wheatstone bridge as used in Lawler et.al model as shown in Figure 4. The impedance of the model is determined by the block marked with black dashed line. The impedance formula will be elaborated starting from Equation 3 to Equation 6, and the final formula of the impedance will be shown in Equation 6.

Bulletin of Electr Eng and Inf, Vol. X, No. X, May 2021: xx - xx

.

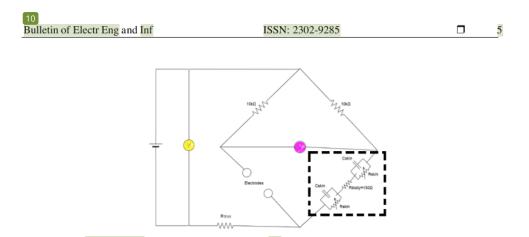


Figure 4. The proposed equivalent circuit for simulation is blocked with the black dashed line.

$$Z = \frac{R_{skin} \cdot X_c}{\sqrt{R_{skin}^2 + X_c^2}} \tag{3}$$

$$X_C = \frac{1}{2\pi f C_{skin}} \tag{4}$$

$$Z = \frac{R_{skin} \cdot (\frac{1}{2\pi f C_{skin}})}{\sqrt{R_{skin}^2 + (\frac{1}{2\pi f C_{skin}})^2}}$$
(5)

Therefore, the impedance for this circuit is:

$$Z = \frac{R_{skin} \cdot (\frac{1}{2\pi f C_{skin}})}{\sqrt{R_{skin}^2 + (\frac{1}{2\pi f C_{skin}})^2}} + \frac{R_{skin} \cdot (\frac{1}{2\pi f C_{skin}})}{\sqrt{R_{skin}^2 + (\frac{1}{2\pi f C_{skin}})^2}} + R_{body}$$
(6)

Table 1 shows that models from Lawler et.al and Keller & Kuhn include capacitance and resistance nature of skin, in which the equivalent circuit can be solved for the impedance and the impedance is affected by changes in frequency. Impedance formula of both Lawler et.al and Keller & Kuhn models are shown in Equations 1 to 6 and from the formula can be inferred that impedance is inversely proportional to frequency. Moineau's is the least model among those previous models and will be neglected later in our simulations.

Table 1. Performance characteristic between three previous models and the proposed model.

Model / Parameter	Impedance	Capacitance	Resistance	Frequency
Lawler et.al	√	√	✓	✓
Moineau et.al	×	×	✓	×
Keller & Kuhn	✓	✓	✓	\checkmark
Proposed Model	✓	✓	✓	✓

Table 2. Simulation parameters.

Models	R _{skin} (KΩ) (fixed)	R _{skin} (KΩ) (variable)	$R_{\text{body}}(\Omega)$	$R_b(\Omega)$	$R_c(K\Omega)$	C _{skin} (nF) (variable)
Proposed Model	10	10-100	150	-	-	83-251
Lawler et.al	10	10-100	-	-	-	83-251
Keller and Kuhn	10	10-100	-	150	1	83-251

Simulation Analysis of Equivalent Circuit Model of Skin-Electrode Impedance... (J.W. Simatupang)

3. Simulation Results and Analysis

In this section, the results of simulation from the proposed model, Lawler et.al, and Keller & Kuhn models will be elaborated. Table 2 above shows the parameters used to simulate the proposed model, Lawler et.al and Keller & Kuhn model, for it to be further analyzed. The frequency is chosen variably from 10 to 150 Hz.

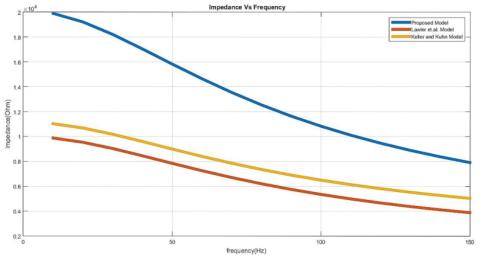
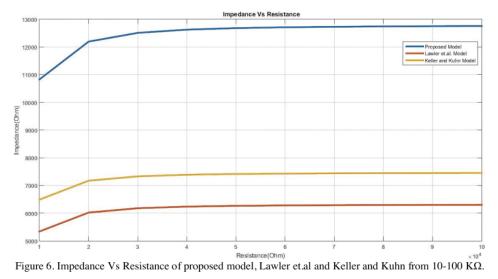


Figure 5. Impedance Vs Frequency of proposed model, Lawler et.al and Keller and Kuhn from 10-150 Hz.

In the first, impedance vs frequency is simulated by varying the frequency with ranging from 10 to 150 Hz. The results of simulation are shown in Figures 5, 6, and 7. In Figure 5, we can see that the highest impedance of the proposed model is 19.990 K Ω and the lowest impedance of 7.911 K Ω , Lawler et.al model showing highest impedance of 9.877 K Ω and lowest impedance of 3.881 K Ω and Keller and Kuhn Model shows highest impedance of 11.027 K Ω and lowest impedance of 5.031 K Ω . From these results, it can be concluded that the impedance is inversely proportional to frequency.



Bulletin of Electr Eng and Inf, Vol. X, No. X, May 2021: xx - xx

6

Bulletin of Electr Eng and Inf

Then, impedance vs resistance is simulated by varying resistance ranging from 10 K Ω to 100 K Ω , and frequency of 100 Hz. Proposed model results in the increment of 1.365 K Ω from 10 to 20 K Ω , Lawler et.al and Keller & Kuhn model showing increment of 0.683 K Ω from 10 to 20 K Ω , from 30 K Ω to 100 K Ω just small increment occur. The results of simulation are shown in Figure 6.

Finally, impedance vs capacitance of proposed model, Lawler et.al and Keller & Kuhn are simulated by varying the capacitance value ranging from 83 to 251 nF. The proposed model yields the highest impedance of 17.883 K Ω and lowest impedance of 10.860 K Ω , Lawler et.al model highest impedance is 8.867 K Ω and lowest impedance of 5.355 K Ω , Keller & Kuhn model highest impedance is 10.017 K Ω and lowest impedance of 6.505 K Ω . The results are shown in Figure 7. From the results, we can conclude that capacitance is inversely proportional to impedance.

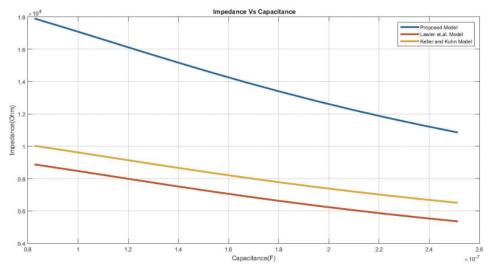


Figure 7. Impedance Vs Capacitance of proposed model, Lawler et.al and Keller and Kuhn from 83-251 nF.

In this research, the frequency is affecting the accuracy of the measurement on high frequency which can cause error due to the changing current distribution beneath electrodes surface and low frequency error due to the impedance, causing $V \neq 0$ [27]. Low freq[4] ncy impedance can be used for indicating skin burn [28]. In addition, at low frequency impedance reflects the resistive prop[4] ties of extra-cellular environment. Higher frequency impedance is reflecting both resistive and capacitive properties of intra and extra-cellular environments. The overall impedance may state the clinical state of human skin [29]. The overall impedance of human tissue is in K Ω range, measurement made on human impedance using high accuracy bioimpedance measurement system by this following set up, frequency ranging from 24 KHz to 391 KHz, excitation current of 10 μ A, and resulting 37 K Ω of impedance [30].

From the results comparison of proposed model, Lawler et.al and Keller & Kuhn model, by variation in frequency, resistance and capacitance, all of the impedance results showing that the proposed model shows the highest impedance, followed by Keller & Kuhn, then Lawler et.al. The proposed model showed a refinement in terms of impedance. Having this quality, proposed model is expected to deliver better comfort stimulation.

4. CONCLUSIONS AND FUTURE WORKS

Results yield from our simulations show that the proposed model has the highest impedance, followed by Keller & Kuhn, then Lawler et.al models. Therefore, the proposed model is considered to be the refinement product compared to other models and expected to deliver better comfort in electrical stimulation. For future works, adding low pass filter might be good to give a better signal to noise (S/N) ratio. Also, by modeling the equivalent circuit using Thevenin scheme, with including the parallel RC circuit and resistance.

ACKNOWLE 21 GEMENTS

Thank to Research Institute and Community Service of President University for supporting our work.

Simulation Analysis of Equivalent Circuit Model of Skin-Electrode Impedance... (J.W. Simatupang)

7

REFERENCES

- N. Sha, L. Kenney, B. Heller, A. Barker and D. Howard, "A Finite Element Model to Identify Electrode Influence [1] on Current Distribuution in the Skin," Artificial Organs, vol. 32, pp. 639-43, 2008.
- [2] T. Keller and A. Kuhn, "Electrodes for transcutaneous (surface) Electrical Stimulation," Journal of Automatic Control, University of Belgrade, vol. 18, no. 2, pp. 35-45, 2008.
- B. Moineau et.al, "Garments for Functional Electrical Stimulation: Design and Proofs of Concept," Journal of [3] Rehabilitation and Assistive Technologies Engineering, vol. 6, pp.1-15, 2019.
- [4] M. Sacilotto et.al, "A Simpler and Shorter Neuromuscular Electrical Stimulation Protocol Improves Functional Status and Modulates Inflammatory Profile in Patients with End-Stage Congestive Heart Failure," International Journal of Cardiovascular Sciences, vol. 30, no. 6, pp. 484-494, 2017. J. L. V. Luna, M. Krenn, J. A. C. Ramirez and W. Mayr, "Dynamic Impedance Model of the Skin-Electrode
- [5] Interface for Transcutaneous Electrical Stimulation," Plos One, pp. 1-15, 2015.
- K. Zhu, L. Li, X. Wei and X. Sui, "A 3D Computational odel of Transcutaneous Electrical Nerve Stimulation for [6] Estimating Aß Tactile Nerve Fiber Excitability," Frontiers in Neuroscience, vol. 11, p. 250, 2017.
- S. Pitou, F. Wu, A. Shafti, B. Michael, R. Stopforth and M. Howard, "Embroidered Electrodes for Control of [7] Affordable Myoelectric Prostheses," King's College London, 2018.
- [8] H. Zhou, Y. Lu, W. Chen, Z. Wu, H. K. L. Zou and L. Guanglin, "Stimulating the Comfort of Textile Electrodes in Wearable Neuromuscular Electrical Stimulation," Sensors, vol. 15, No. 7, pp. 17241-17257, 2015
- [9] C. Mavridis, "Internship report Engineering Assistant - Wearable technology," Manchester Metropolitan University (MMU), Manchester, United Kingdom, 2019.
- [10] M. Qassem and P. Kyriacou, "Review of Modern Techniques for the Assessment of Skin Hydration," Cosmetics, vol. 6, no. 19, 2019.
- [11] V. Zuang, C. Rona, F. Distante and E. Berardesca, "The Use of a Capacitance Device to Evaluate The Hydration of Human Skin.," J Appl. Cosmetol., 1997.
- [12] C. Bontozoglou and P. Xiao, "Applications of Capacitive Imaging in Human Skin Texture and Hair Analysis," Appl. Sci., vol. 10, no. 256, 2020.
- [13] L. L. Baker, B. R. Bowman and D. R. McNeal, "Effects of Waveform on Comfort During Neuromuscular Electrical Stimulation," Clinical Orthopaedics and Related Research, 1987.
- [14] J.C. Lawler, M. J. Davis and E. C. Griffith, "Electrical Characteristics of The Skin: The Impedance of The Surface Sheath and Deep Tissues," J. Investigative Dermatology, Vol.34, Issue 5, pp.301-308, May 1960.
- [15] A. Albulbul, "Evaluating Major Electrode Types for Idle Biological Signal Measurements for Modern Medical Technology," Bioengineering, vol. 3, no. 20, 2016.
- [16] J. Kim and G. Yoon, "Study on Reusable Electrodes for Personal Electrocardiography," Journal of Sensor Science and Technology, vol. 27, no. 5, 2018.
- D. Tyler and C. Mavridis, "Wearable FES Electrodes," in MDPI, Basel, Switzerland, 2019. [17]
- S. Zsikó, E. Csányi, A. Kovács, M. B. Szucs, A. Gácsi and S. Berkó, "Methods to Evaluate Skin Penetration In [18] Vitro," Sci. Pharm, vol. 87, no. 19, 2019.
- [19] J. M. Abdo, N. A. Sopko and S. M. Milner, "The applied anatomy of human skin: A model for regeneration," Wound Medicine, vol. 28, 2020.
- [20] F. Lu, C. Wang, R. Zhao, L. Du, Z. Fang, X. Guo and Z. Zhao, "Review of Stratum Corneum Impedance Measurement in Non-Invasive Penetration Application," Biosensors, vol. 8, no. 31, pp. 1-20, 2018.
- H. Yousef and S. Sharma, "Anatomy, Skin (Integument), Epidermis," National Institutes of Health, 2017. [21]
- C. Gorzelanny et.al, "Skin Barriers in Dermal Drug Delivery: Which Barriers Have to Be Overcome and How Can [22] We Measure Them?" Pharmaceutics, vol. 12, no. 684, pp. 1-31, 2020.
- L. Davis, "A Cellular Model of the Electrical Characteristics of Skin," University of Southampton, 2018. [23]
- Y. A. Chizmadzhev, A. V. Indenbom, P. I. Kuzmin, S. V. Galichenko and J. C. Weaver, "Electrical Properties of [24] Skin at Moderate Voltages: Contribution of Appendageal Macropores," Biophysical Journal, vol. 74, 1998.
- T.-Y. Wu, B. Wang, J.-Y. Lee, H.-P. Shen, Y.-C. Wu, Y.-A. Chen, P.-S. Ku, M.-W. Hsu, Y.-C. Lin and M. Y. [25] Chen, "CircuitSense: Automatic Sensing of Physical Circuits and Generation of Virtual Circuits to Support Software Tools," UIST, 2017.
- [26] Κ. Hoffmann, "Applying The Wheatstone Bridge Circuit," [Online]. Available: http://eln.teilam.gr/sites/default/files/Wheatstone%20bridge.pdf. [Accessed 28 03 2021].
- [27] O. Ibrahim, S. M. Hassan, A. Abdulkarim, M. F. Akorede, S. Amuda and A.Y., "Design of Wheatstone Bridge Based Thermistor Signal Conditioning Circuit for Temperature Measurement," Journal of Engineering Science and Technology Review, vol. 12, 2019.
- L. Yang et.al, "The Frequency Spectral Properties of Electrode-Skin Contact Impedance on Human Head and Its [28] Frequency-Dependent Effects on Frequency-Difference EIT in Stroke Detection from 10Hz to 1MHz," Plos One, pp. 1-21, 2017.
- [29] K. A. Sillay et.al, "Long-Term Surface Electrode Impedance Recordings Associated with Gliosis for a Closed-Loop Neurostimulation Device," Ann Neurosci, vol. 25, pp. 289-298, 2018.
- [30] U. Birgersson, "Electrical Impedance of Human Skin and Tissue Alterations: Mathematical Modeling and Measurements," Karolinska Institutet, 2012.

Bulletin of Electr Eng and Inf, Vol. X, No. X, May 2021: xx - xx

Simulation Analysis of Equivalent Circuit Model of Skin-Electrode Impedance

ORIGINA	ALITY REPORT				
SIMILA	0% ARITY INDEX	7% INTERNET SOURCES	6% PUBLICATIONS	5% STUDENT PA	PERS
PRIMAR	Y SOURCES				
1	Submitt Student Pape	ed to Universiti	Teknologi MA	RA	3%
2	"Modelii cascade Bulletin	adma Panigrahi, ng and simulatio d H-bridge grid- of Electrical Eng tics, 2019	on of three ph tied PV inverte	ases	1 %
3	eprints.s	soton.ac.uk			1%
4	of intact	gersson. "Non-i skin: mathema ents", Physiolog 011	tical modeling	and	1 %
5	umpir.u	mp.edu.my			1%
6	www.ict	open2013.nl			1%

7	www.slclaserclinics.com	<1%
8	L Anggraini. "Failure analysis of S50C carbon steel applied for fine boring transmission system", IOP Conference Series: Materials Science and Engineering, 2018 Publication	<1 %
9	WWW.answers.com Internet Source	<1%
10	Submitted to Multimedia University Student Paper	<1%
11	Zhou, Hui, Yi Lu, Wanzhen Chen, Zhen Wu, Haiqing Zou, Ludovic Krundel, and Guanglin Li. "Stimulating the Comfort of Textile Electrodes in Wearable Neuromuscular Electrical Stimulation", Sensors, 2015. Publication	<1%
12	Submitted to Capital University Student Paper	<1%
13	ijece.iaescore.com Internet Source	<1%
14	Tahereh Jasemi Zad, Maryani Paramita Astuti, Lokesh P. Padhye. "Fate of Environmental Pollutants", Water Environment Research, 2018 Publication	<1%

15	Submitted to University of Southampton Student Paper	<1%
16	www.courage-khazaka.de	<1%
17	www.mdpi.com Internet Source	<1%
18	Anas Albulbul. "Evaluating Major Electrode Types for Idle Biological Signal Measurements for Modern Medical Technology", Bioengineering, 2016 Publication	<1%
19	Submitted to Higher Education Commission Pakistan Student Paper	<1%
20	worldwidescience.org	<1%
21	www.internetworkingindonesia.org	<1 %
22	www.japsonline.com	<1%

Exclude quotes	On
Exclude bibliography	On

Exclude matches

Off